 ROBL-CRG	Experiment title: <i>In-situ</i> XRD during thermal cycling of Ni-Ti Shape Memory Alloy	Experiment number: 20_02_626
Beamline: BM20	Date of experiment: from: 18.09.2004 to: 21.09.2004	Date of report: 19.11.2004
Shifts: 9	Local contact(s): Dr. Norbert Schell	<i>Received at ESRF:</i>
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Report

Aim

The aim of the experiment was to analyse the structural evolution during *in-situ* annealing of Nickel-Titanium (Ni-Ti) SMA subjected to thermal/mechanical treatments.

Experimental Methodology

The material in study was Ti-rich (Ti 51 at%) NiTi SMA extracted from a 2 mm thick plate, in strain annealed conditions and supplied by Memory-Metalle GmbH, Germany. The samples were analyzed in the following conditions: (i) as-received (AR), (ii) heat treated at 500°C (HT), (iii) heat treated at 500°C followed by 10% thickness reduction by cold rolling (HT + CW10%) and (iv) heat treated at 500°C followed by 40% thickness reduction by cold rolling (HT + CW40%). The heat treatment (HT) was performed by holding the specimen at 500°C for 30 minutes and subsequently quenching in water at room temperature. The samples were subjected to chemical etching (10% vol HF + 45% vol HNO₃ + 45% vol H₂O) in order to remove the oxide layer as well as the layer deformed during the cutting operation.

XRD analysis was performed at ROBL/BM20 of ESRF for the *in-situ* high temperature $\theta/2\theta$ scans and texture analysis. *In-situ* XRD analysis during annealing has been carried out using x-rays of wavelength 1.54 Å and a vacuum furnace with a hemispherical Be-dome evacuated to a pressure less than 2×10^{-6} mbar. The furnace was installed on the ϕ circle (azimuthal orientation) of the six-circle goniometer. The pole figures have been determined for $-85^\circ < \phi < +5^\circ$ and $0^\circ < \chi < +54^\circ$. The rolling direction (RD) is aligned with $\phi = -55^\circ$. The structural evolution during annealing up to 800°C was observed by *in-situ* XRD.

Results

All the samples are in the martensitic state, at room temperature before *in-situ* high temperature analysis (scan 1 in Fig. 1a-d). The structural evolution while heating (Fig. 1 for the scans up to 400°C, where the recrystallisation is completed, and Fig. 2 for the full range of temperatures) and cooling (Fig. 3) was followed by *in-situ* XRD. For the HT+CW10% and HT+CW40% samples, overlapping of the martensite peaks are observed. The XRD scans in $\theta/2\theta$ mode (Figs 1 and 2) show a clear variation in peaks corresponding to the structural evolution. In Figs 1c-d, for HT+CW10% and HT+CW40%, it is seen that the full transformation to austenite occurs only when the sample is heated above 100°C. The recrystallisation temperature is close to 350°C, which is in agreement with other results [1-4]. At higher temperatures (above 600°C) a significant structural evolution takes place, illustrated by the increased austenitic peak intensity in both HT and HT+CW40% samples (Figs 2b and c), and the growth of Ti₂Ni precipitates. The structural evolution during cooling (Fig. 3) shows B2→B19' in the AR sample (after heating up to 800°C) and B2→R→B19' in the

HT+CW10% sample (after heating up to 400°C). These results are in agreement with previous results [3-6], where the R-Phase formation is gradually suppressed with increasing annealing temperatures, leading to one step transformation as it is detected by DSC analysis.

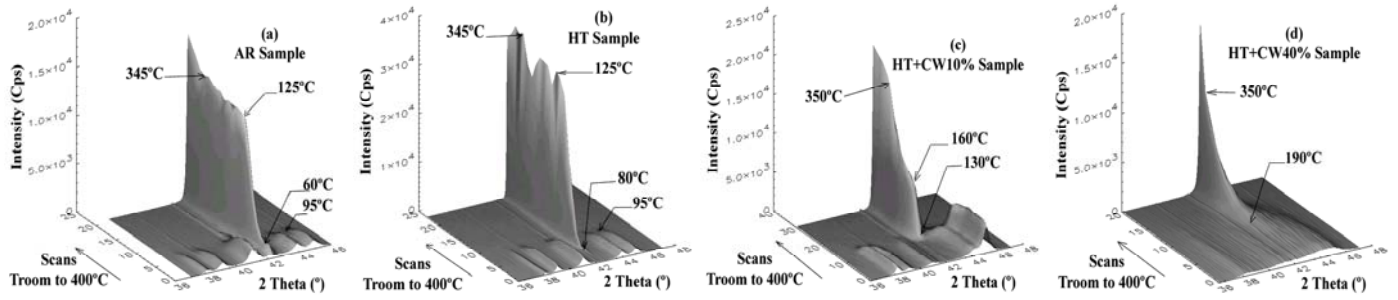


Fig. 1: XRD spectra during the *in-situ* high temperature analysis for AR, HT, HT+CW10% and HT+CW40% samples while heating up to 400°C.

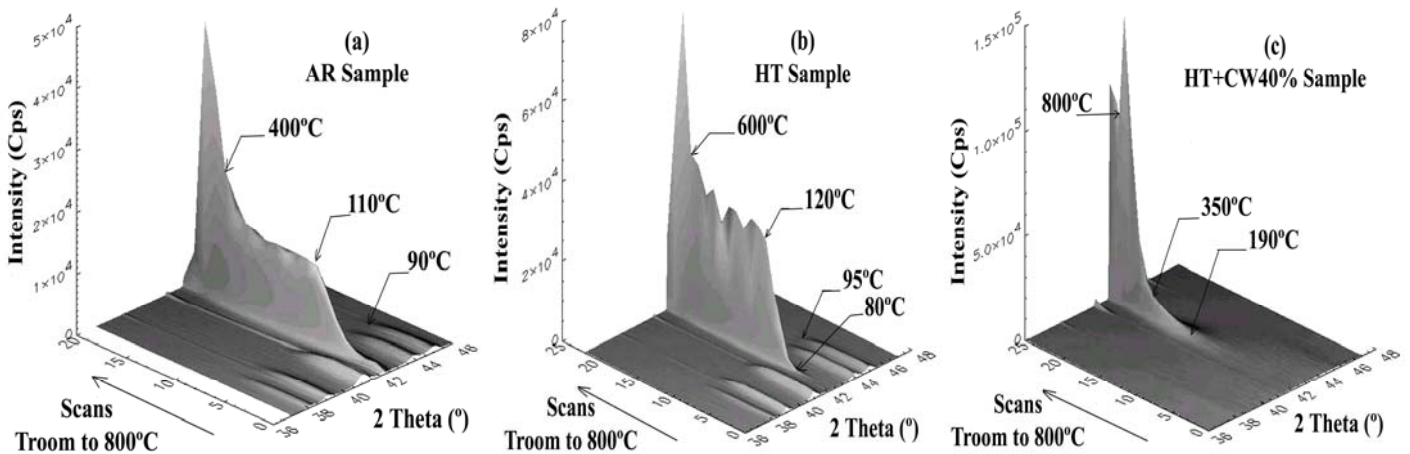


Fig. 2: XRD spectra evolution during the *in-situ* high temperature analysis for AR, HT and HT+CW40% samples while heating up to 800°C.

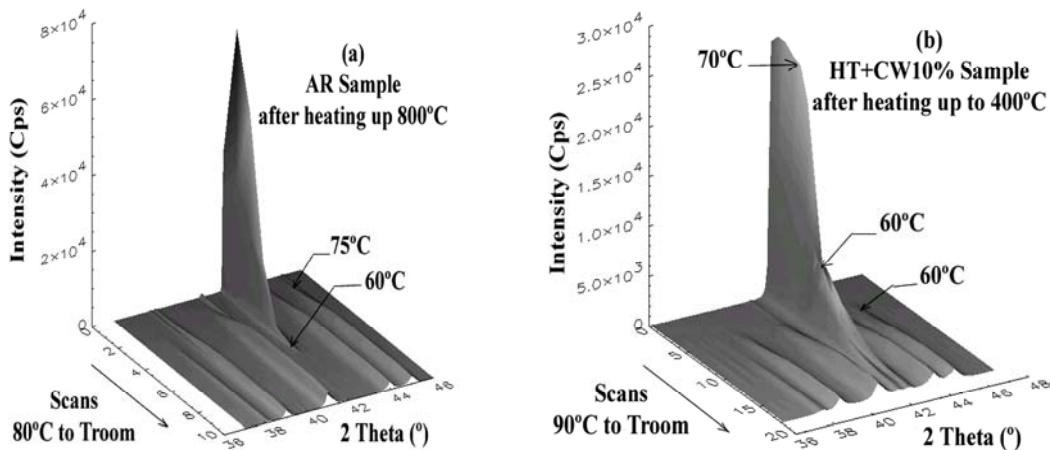


Fig. 3: XRD spectra evolution during the *in-situ* high temperature analysis for AR and HT+CW10% samples after heating up to 800°C and 400°C, respectively.

The texture evolution during the *in-situ* high temperature XRD analysis of the HT and HT+CW40% samples is shown in Figs 4 and 5, respectively.

Annealing up to 350°C (Figs 4a-c), gives no significant modifications in the $\{111\}\langle 110 \rangle$ austenite texture components of AR and HT samples; recrystallisation in HT+CW40% sample is completed at 350°C (Fig. 1d) [2-4]. Between 400° and 500°C (Figs 4d-f and 5a), there are texture evolutions in the direction of $\{110\}\langle 110 \rangle$ austenite texture components [2-4, 7-9]. Above 600°C, anomalous grain growth of austenite is starting to occur.

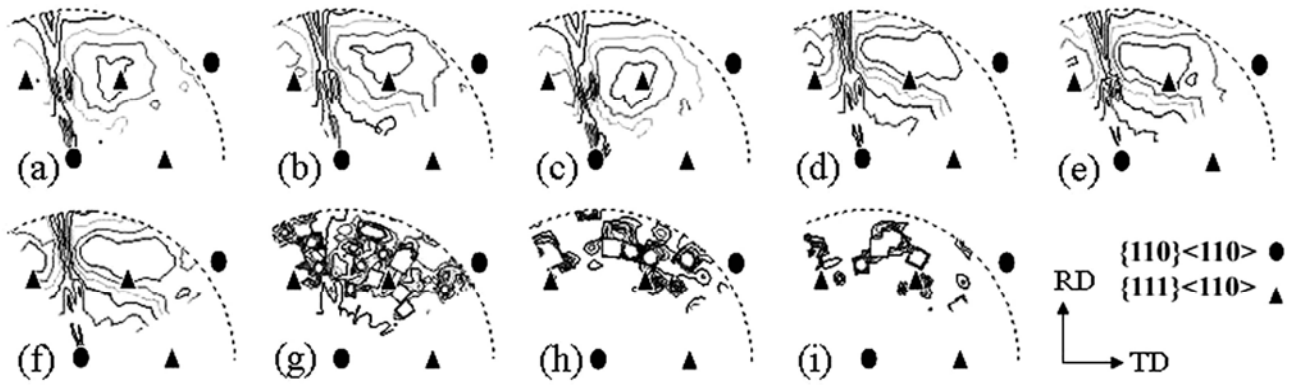


Fig. 4: Austenite (110) Pole Figures – HT sample – (a) 250°C, (b) 300°C, (c) 350°C, (d) 400°C, (e) 450°C, (f) 500°C, (g) 600°C, (h) 700°C and (i) 800°C during the in-situ high temperature XRD.

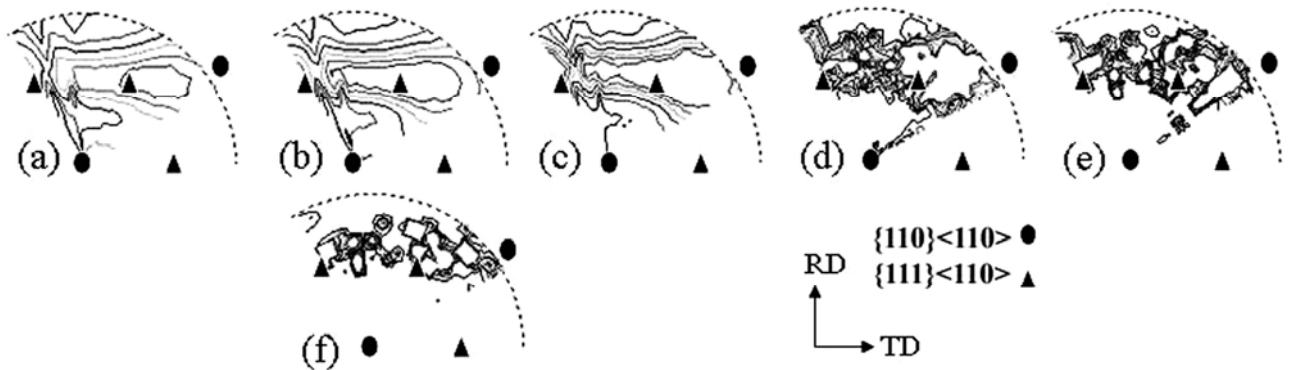


Fig. 5: Austenite (110) Pole Figures – HT+CW40% sample – (a) 400°C, (b) 450°C, (c) 500°C, (d) 600°C, (e) 700°C and (f) 800°C during the in-situ high temperature XRD.

Conclusions:

- (1) The thermal / mechanical treatments significantly affect the structural evolution in the Ti-rich NiTi SMA.
- (2) High annealing temperature develops {110}<110> austenite texture component in Ti-rich NiTi SMA.
- (3) Above 500°C, precipitation of Ti_2Ni takes place, and above 600°C a tendency for anomalous grain growth appears.

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